



Hydrate and Hydrate Inhibition
by Sekar Darujati

- Definition of gas hydrate
- Hydrates in pipeline
- Hydrate prediction
- Hydrate prevention
- Hydrate inhibition
- Example problem

What is Gas Hydrate?

- Clathrate: HC molecules are entrapped in a cage structured composed of H₂O molecules
- The structure of hydrate depends on the type of HC molecules
- Hydrate can form at temperatures above water freezing temperature
- Favored conditions: low T, high P (water has to be present)
- Time dependent – rate depends on the gas composition, the presence of nucleation sites, flow turbulence, etc.

Hydrate former:

N₂

CO₂

H₂S

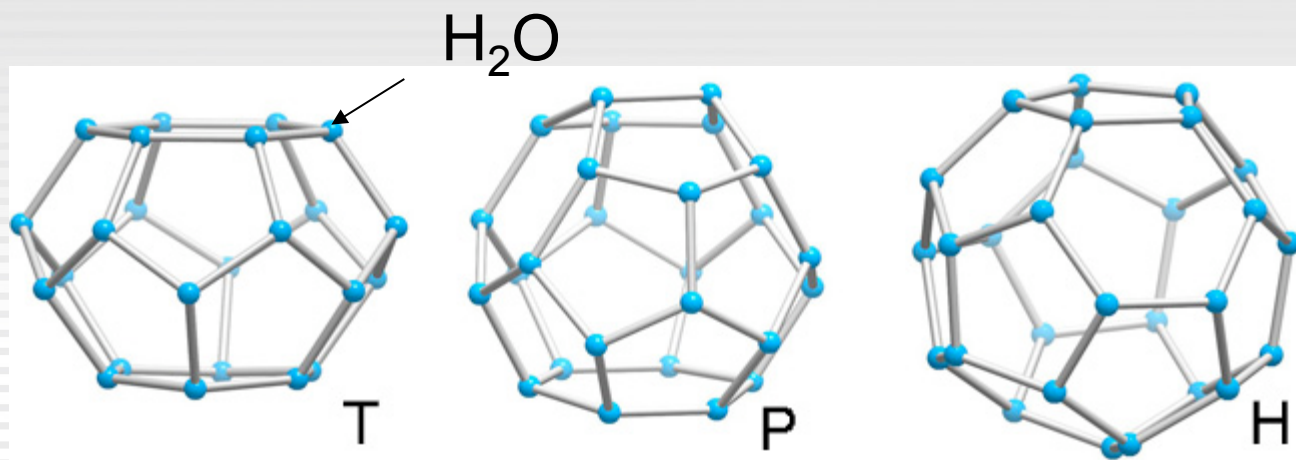
CH₄

C₂H₆

C₃H₈

i-C₄H₁₀

n-C₄H₁₀



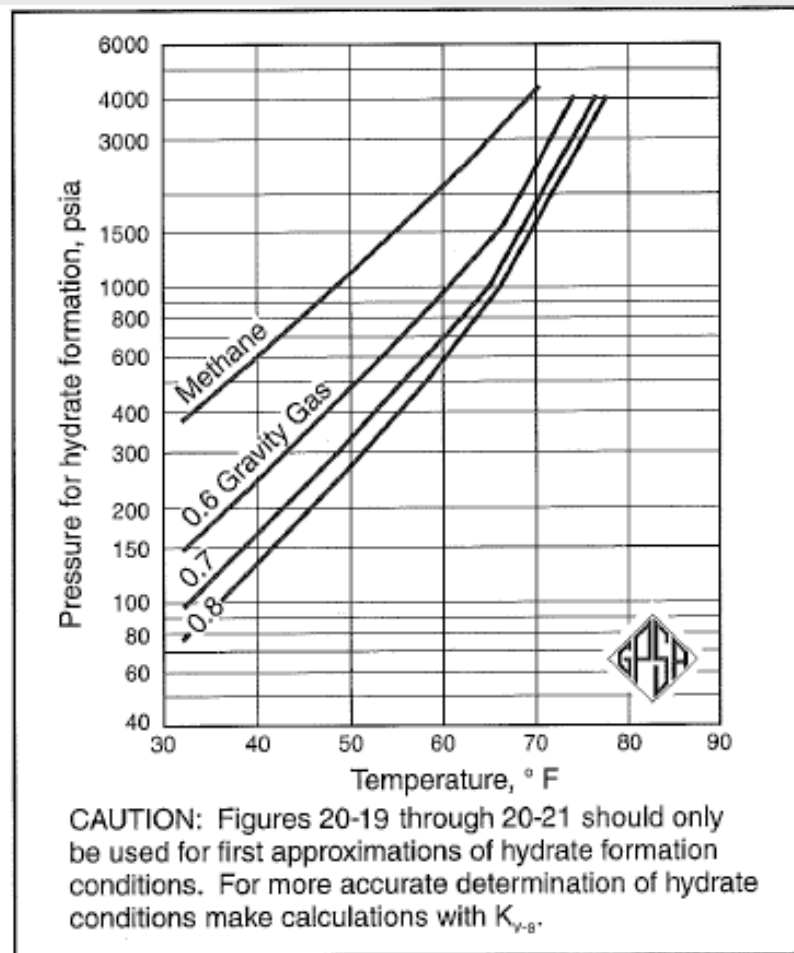
ConocoPhillips

Hydrates in Pipelines

- When will it form? T drops below dew point AND hydrate formation T
- Typical locations:
 - Low points in the lines/pockets of water
 - Large pressure drop:
 - Orifices, sudden enlargement on pipeline, elbows, etc.
- Problems: block pipeline, cause pipe rupture around the pipe bend, pipe rupture due to high P generated by the plug momentum
- Removal is challenging and dangerous:
 - Large pressure differential across the plug
 - Large release of gas upon melting – especially sour gas
 - Refer to company guidelines for hydrate handling

Prediction of Hydrate Formation

- GPSA chart for quick approximations

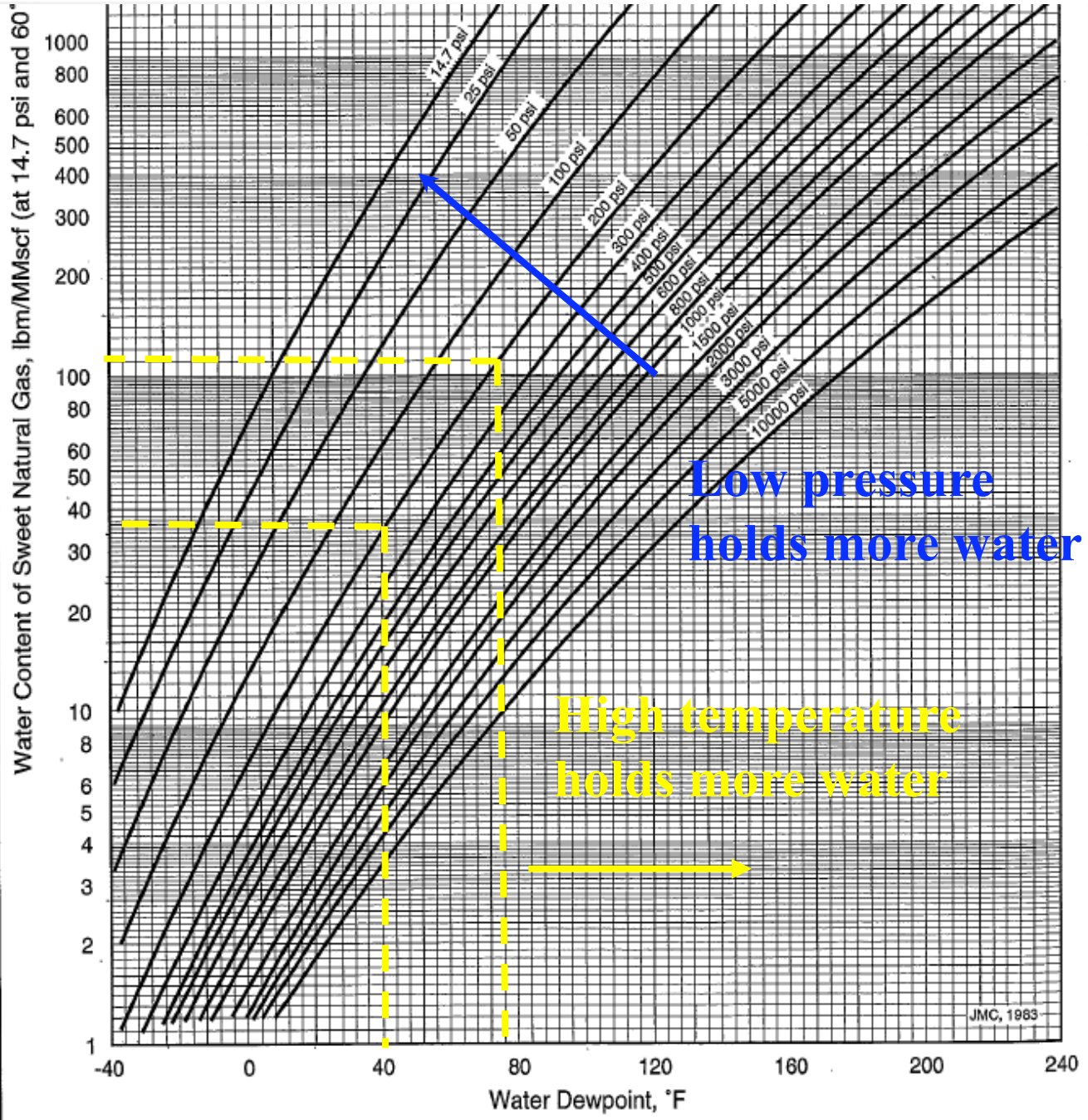


- Katz method using K_{vs} (reliable up to 1,000 psia)
- McLeod-Campbell method (for 5,000 – 6,000 psia)
- EOS → Hysys, ProMax, etc

Hydrate Prevention

- Reducing the P below that of the hydrate formation (for a given T)
- Adding heat: keeping the operating T above the hydrate formation T
- Dehydration: reducing water content in the gas to keep the system above water dew point
- Inhibition: reducing the thermodynamic potential for hydrate formation or modify the rate formation
- Ensure proper design of the system

Water content of natural Gas



McKetta & Wehe, 1958



Other Variables which Affect Water Content of Natural Gas

- Effect of CO₂ and H₂S:
 - Pure CO₂ and H₂S can hold more water than sweet natural gas especially at pressures above 700 psia
 - Corrections should be applied if the gas content CO₂ and/or H₂S above 5% at P > 700 psia

Hydrate Inhibition

- Thermodynamic inhibitors: methanol, glycol (most common)
- Kinetic inhibitors: polymer-based chemicals
- Hammerschmidt's equation is used to predict (thermodynamic) inhibitor concentration:

$$X_R = \frac{(d)(M)}{K_i + (d)(M)} (100)$$

d = depression of hydrate point

X_R = min. wt.% of inhibitor in the liquid phase (rich inhibitor concent.)

M = molecular weight of inhibitor; MeOH = 32

K_i = constant = 2,335 (FPS), 1,297 (SI)

- Inhibitor injection rate:

$$m_I = m_W \left(\frac{X_R}{X_L - X_R} \right)$$

m_I = mass flow of inhibitor solution [lb/d]

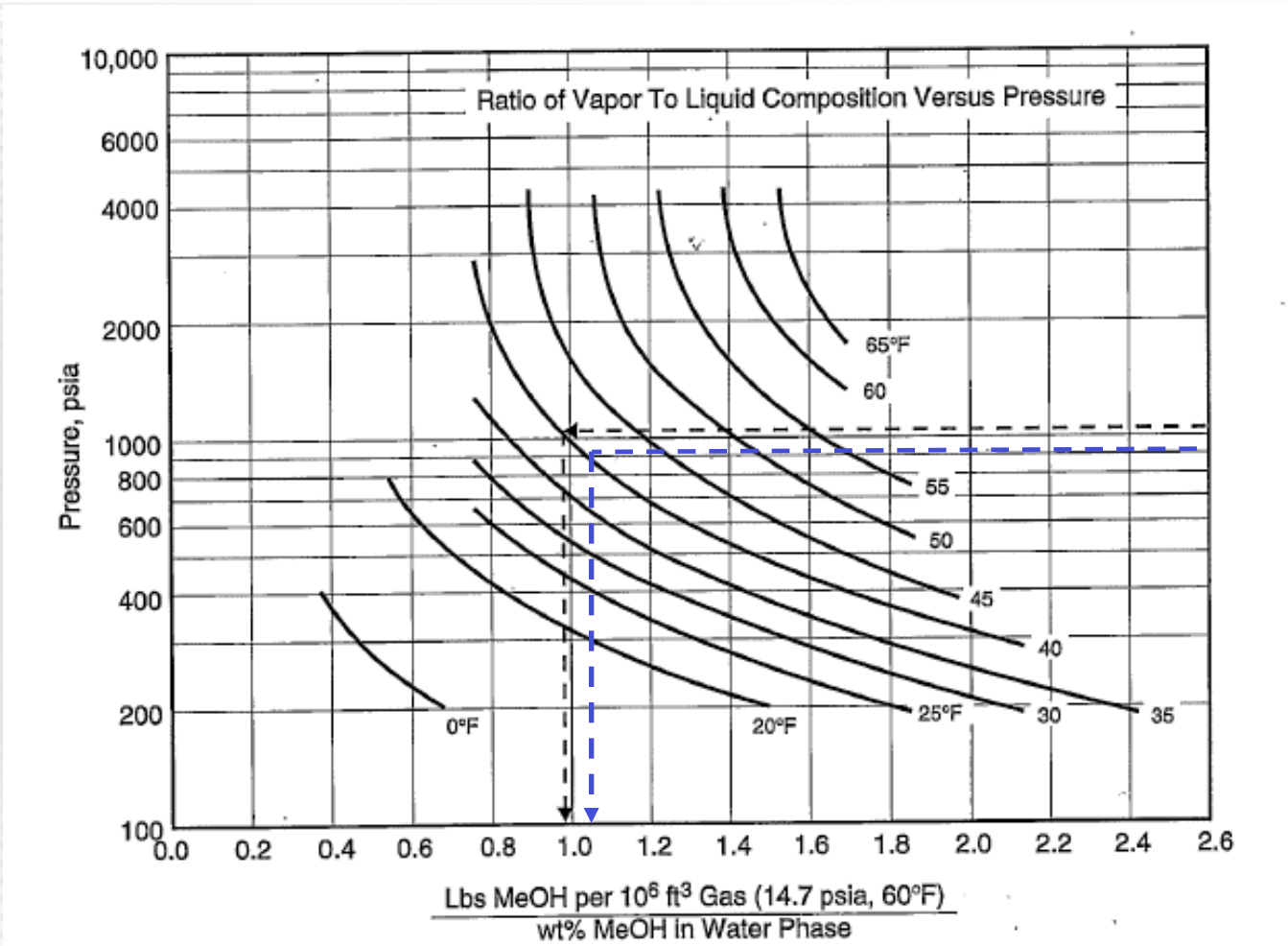
m_W = mass flow of liquid water [lb/d]

X_R = rich inhibitor concentration [wt.%]

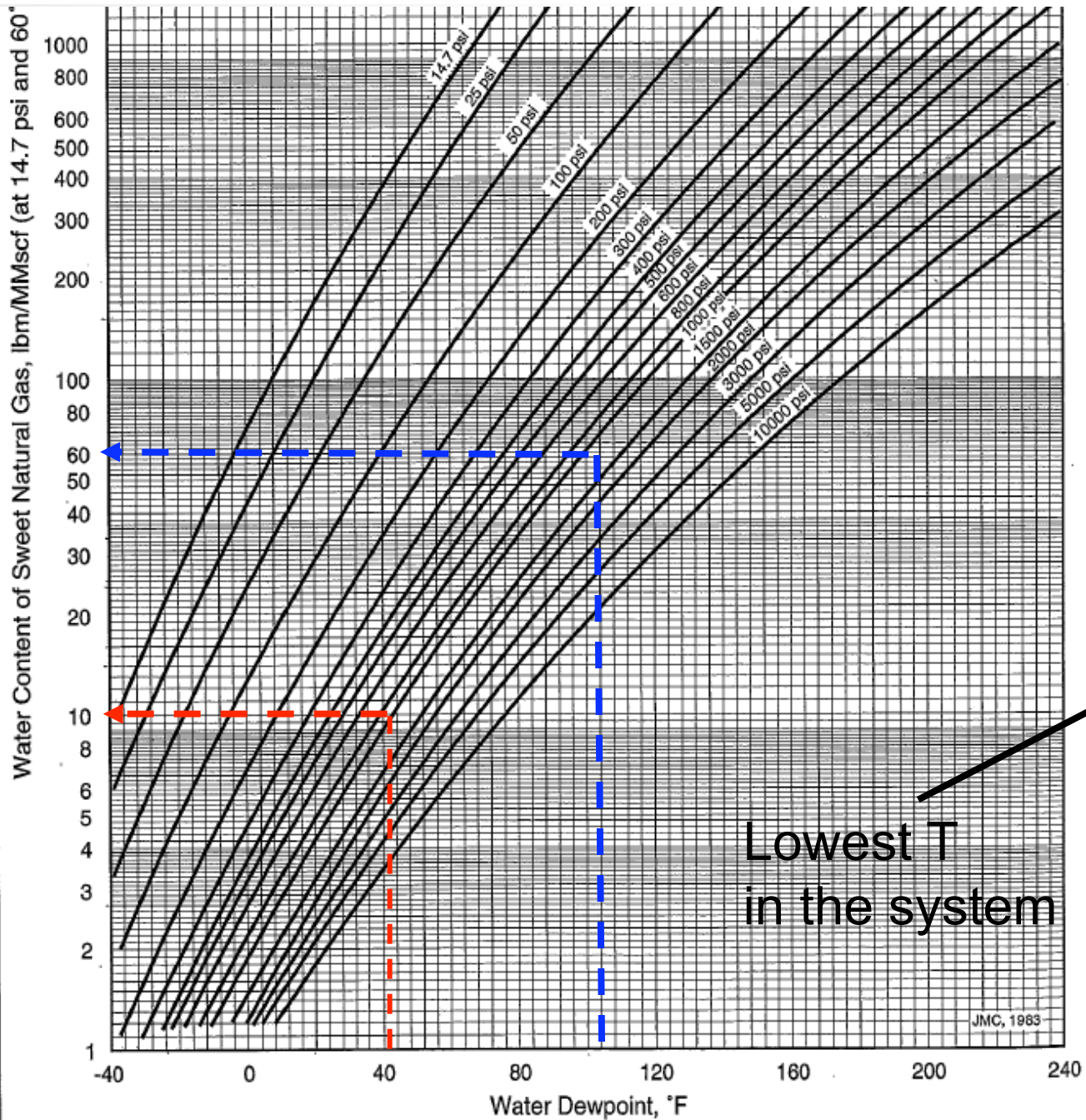
X_L = lean inhibitor concentration [wt.%]; 60 – 80%
for glycol, ~ 95 - 100% for methanol

- Inhibitor losses to the hydrocarbon phase:
 - For glycol → small
 - For methanol → significant

- Methanol losses to HC vapor



- Methanol losses to HC liquid ~ 0.15 lb/bbl (JMC)



Example:

10 MMSCFD (283 e³m³/d) Sweet gas, entering pipeline:

entering pipeline:

P = 1,160 psia

(8,000 kPa)

T = 104°F (40°C)

Gas arrives at the gas plant:

P = 900 psia

(6,205 kPa)

T = 41°F (5°C)

Hydrate T = 63°F

Methanol required to prevent hydrate formation?

ConocoPhillips

- Calculate water content of the gas at the inlet of pipeline (at 1,000 psia, 67°F)
= 60 lb/MMSCF (1,000 kg/10⁶ std m³)
- Calculate water content at the inlet of gas plant (at 900 psia, 41°F)
= 10 lb/MMSCF (170 kg/10⁶ std m³)
- Calculate water condensed
= (60 - 10)lb/MMSCF x 10 MMSCF
= 500 lb/d (235 kg/d) → m_w
- Calculate d (depression of hydrate point)
= 63 - 41 = 22°F (12°C)
- Calculate X_R (rich methanol concent.)
= (22)(32)/{(2,335)+(22)(32)}x100
= 23%

- Calculate methanol injection rate, m_i
 $= (500) \times [(23\%)/(95\% - 23\%)]$
 $= 160 \text{ lb/d (75 kg/d)}$
- Calculate methanol losses to vapor
 $= 1.1 \text{ lb/MMSCF/wt.\%MeOH (from chart)}$
 $= (1.1) \times (10) \times (23)$
 $= 253 \text{ lb/d (114 kg/d)}$
- Total injection rate = $160 + 253 = 413 \text{ lb/d (189 kg/d)}$
Volumetric rate = $(413)/(49.7) \times (7.48)/1440 = \underline{0.04 \text{ USGPM (0.16 L/min)}}$

Questions/Comments?